

معمل هندسة الاتصالات
ثانية إلكترونيات
ترم ثان
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أ/ محمد عيسى + أ/ فراء

Exp ①: VCO

• What is a VCO?

A Voltage Controlled Oscillator is a circuit that Produces [Square wave] whose frequency depends on the i/p voltage.

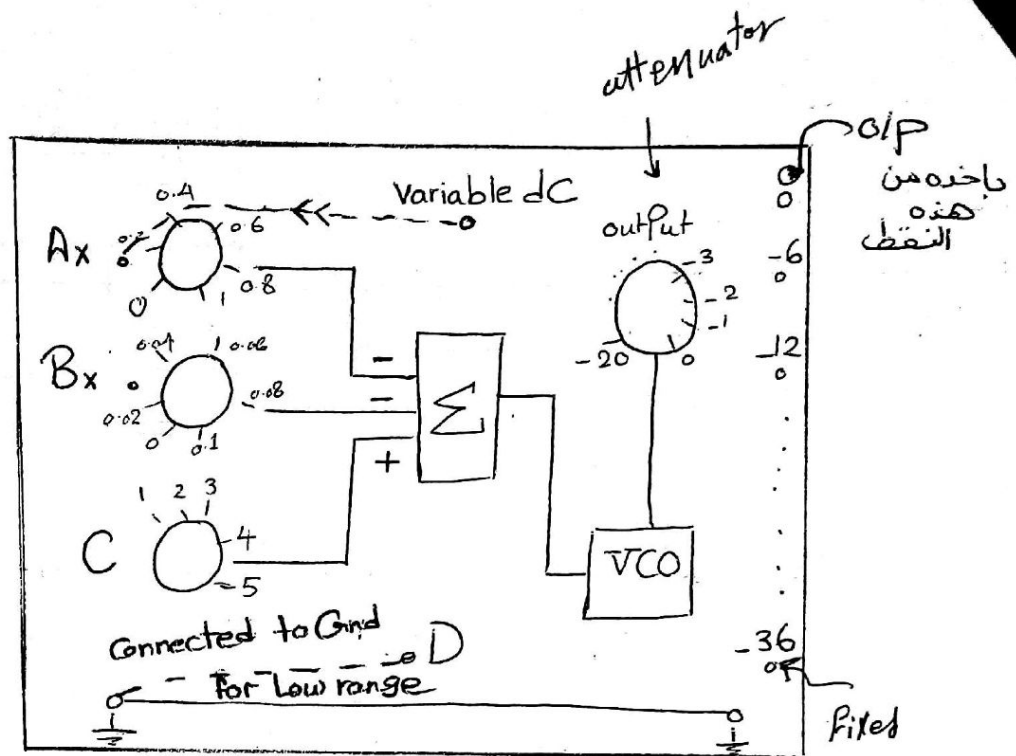
Changing i/p voltage change o/p frequency.

• Applications:

- * Function generator (to get ^{a range of} different frequencies by adjusting a rotator).
- * PLL (Phase-Locked loop)
- * Frequency Synthesizers (a circuit that can be used to generate a range of frequencies)
- * AM modulation (used to [generate the carrier], it is common that the carrier is sinusoidal with a single frequency, a sin signal can be extracted from the square using a filter centered around f_0 which is the square fundamental frequency) "our objective now" $f_c = 465 \text{ KHz}$
- * FM modulator (the VCO achieves the concept of FM as the o/p signal freq. can change with the change in the input [message signal amplitude]).

المودول المستخدمة موجودة في حقيبة عليها 2950. Electronic Comm. وكل module. Trainer

2900 Function generator / Power Supply هو متوافق مع 2950 A VCO هو بها عليه حرف مثلاً ال



• The o/p Square has Amplitude, Frequency.

• How to Control Amplitude?

* Variable attenuator knob

* Fixed o/p/attenuator sockets

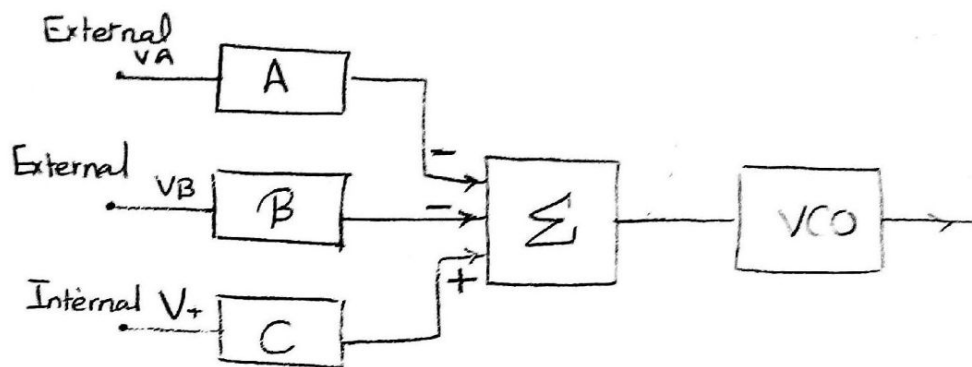
Total att. = Fixed + variable

• How to Control Frequency?

* D → Ground : low range $\approx (1 \text{ KHz} \xrightarrow{C=1} 5 \text{ KHz})$
 → open : high range $\approx (100 \text{ KHz} \xrightarrow{C=5} 1 \text{ MHz})$

* Internal → using C knob [مؤهل ذو شاتبات داخلى]
 there's a potentiometer beside C with ^{different} settings
 that acts as a multiplier to ~~get~~ Control C voltage
 ratio

* External → Ax $V_A \times (0 \rightarrow 1)$ Coarse changes
 Bx $V_B \times (0 \rightarrow 0.1)$ P.



$V_C \uparrow \quad f \uparrow$ لأن إشارة الجهد موجبة

$V_A, V_B \uparrow \quad f \downarrow$ سالبة " " "

Practice 1.1. :- Calibration of VCO

- A, B, ~~not~~ ~~connected~~, variable attenuator = 0
- only change C knob.

change C, observe f

C	① Low range B Cond	② High range Open
	f	f
1	$\approx 1 \text{ KHz}$	
2	$\approx 2 \text{ KHz}$	
3	\vdots	
4		
5	$\approx 5 \text{ KHz}$	1. MHz

Practice 1.2. Use of external Freq. Control Pins

1. D Ground (Low range) C تتب, change A_x , observe F or β_x
- * adjust C for 5 KHz
 - * adjust Power Supply to +4 V.
 - * Connect variable dc socket to A_x .
 - * Try $A=1$ and watch $F \uparrow$ or $\downarrow = ???$
 $A=0.5$ فردة عكسية

* Do the same with B

2. Repeat for D unconnected (ungrounded).

لا داعي لربطه

Practice 1.3. Attenuator ضبط ال F ولاحظ ال attenuation

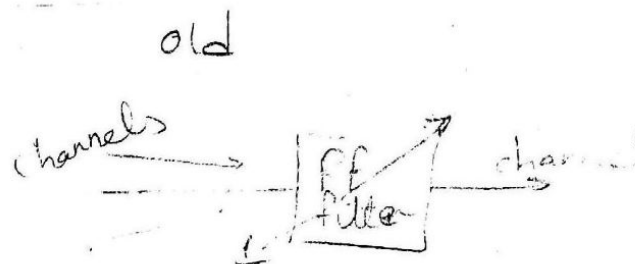
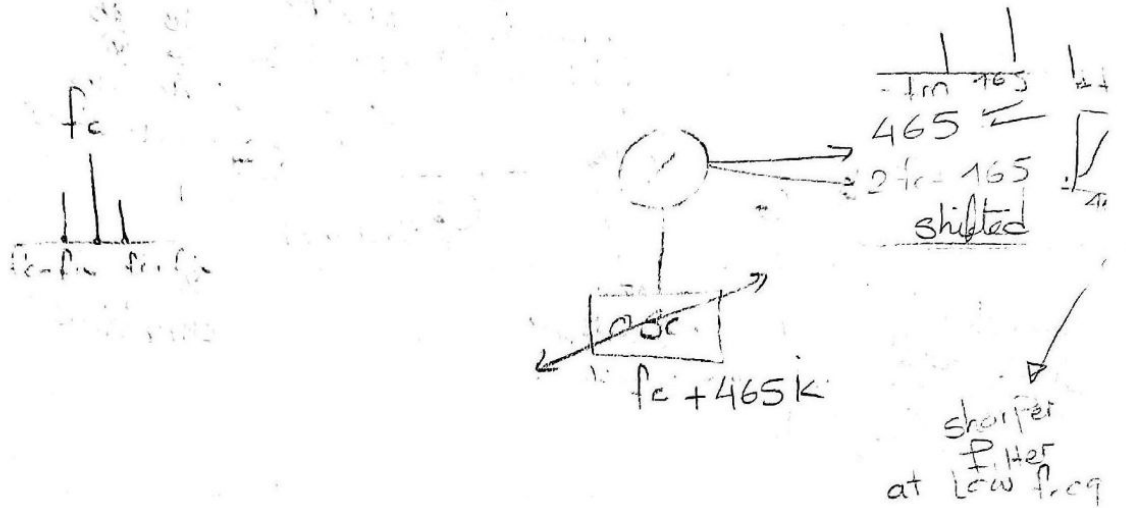
CC

- * A, B, D not connected
- * Set C into dot (AM freq. تتب) or a certain level.

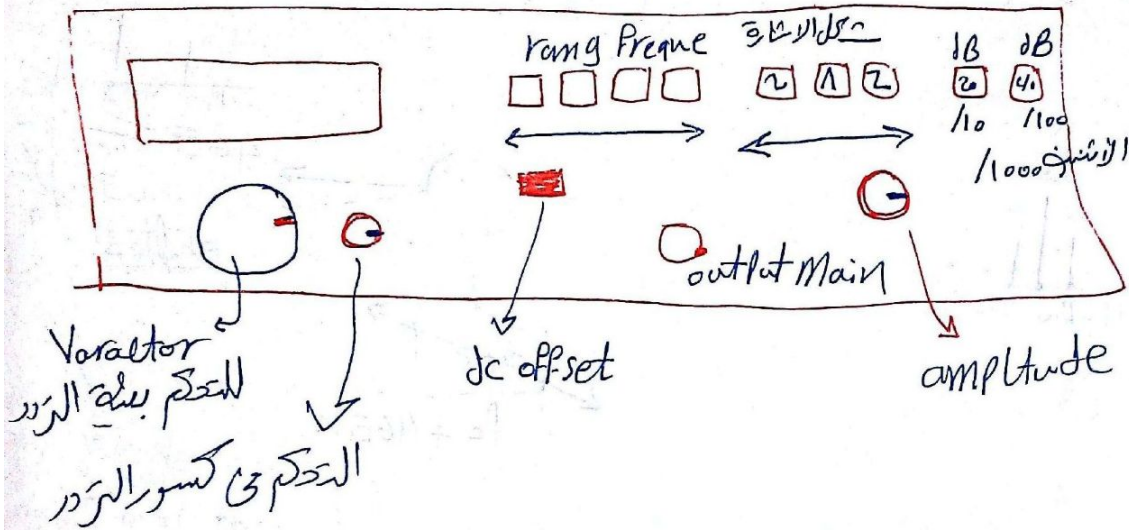
Atten.	V_o o/p p-p	$\frac{V_o}{V}$	$20 \log \frac{V_o}{V}$
0	$V = 1.6V$ for any f	1	0
-3		< 1	-3
-6			
-9			
...			
-36			

VCO is a relaxation osc. made by IC 566 that has square & tri o/p but

في ال Super heterodyne RX التحكم سيكون في oscillator وليس في Filter
 حيث أن ثابت عند 465 K وهو سهل عمليا أن يكون ال OSC هو الباعث variable
 وليس ال Filter كما أن تضخيم البثرة يكون أبسط مع الترددات الأقل



Function generator



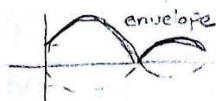
Func

Close my eyes only for
a moment, and the moment's gone

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Exp ③: Full AM (modulation and demodulation)

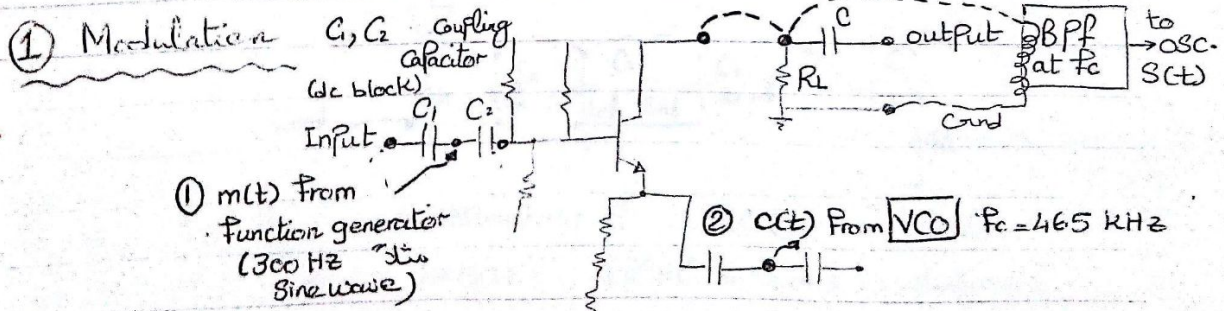
- In analog systems, PM is not available but PSK in digital systems is available.
- AM radio $\rightarrow f_m = 5 \text{ KHz}$
BW of channel $= 2f_m = 10 \text{ KHz}$
- In Full AM $\rightarrow P_c = \frac{2}{3} P_t$ which is wasted power, the useful power is in the DSB.
 - BW $= 2f_m$
 - easy to receive by envelope detector
- μ (modulation index) $= \frac{A_m}{A_c} \rightarrow$ mathematically, $\mu=1$ is accepted
Practically, use $\mu=0.7$ or 0.8



if $\mu > 1$ envelope doesn't represent $m(t)$

$$S(t) = A_c \cdot (1 + \mu m(t)) \cos(2\pi f_c t) \quad \text{or} \quad c(t) \cdot (1 + \mu m(t))$$

- We will use non-linear device for AM mod. (transistor)





$m(t) \rightarrow$ Base
 $c(t) \rightarrow$ emitter
 $s(t) \rightarrow$ collector

$$I_c = I_s (e^{V_{BE}} - 1)$$

$$e^x = 1 + x + \frac{x^2}{2!} + \frac{x^3}{3!} + \dots \quad (\text{Maclaurin Series})$$

$$I_c = I_s + I_1 V_{BE} + I_2 V_{BE}^2 + I_3 V_{BE}^3 + \dots$$

$$\uparrow \quad \begin{matrix} M^2(f) \text{ at } 2f_m \\ m^2(t) = A m^2 \cos^2(2\pi f_m t) \end{matrix}$$

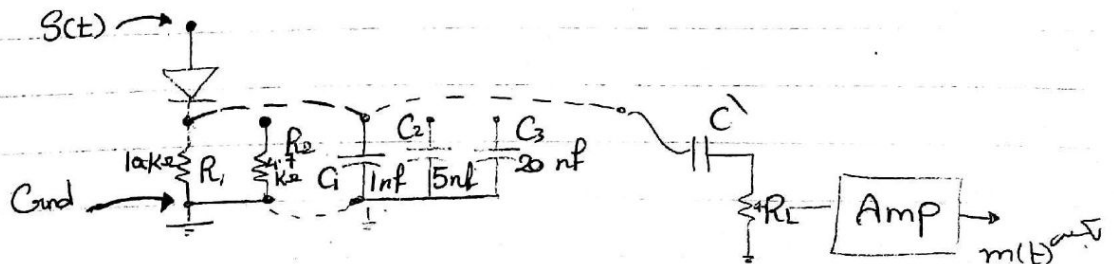
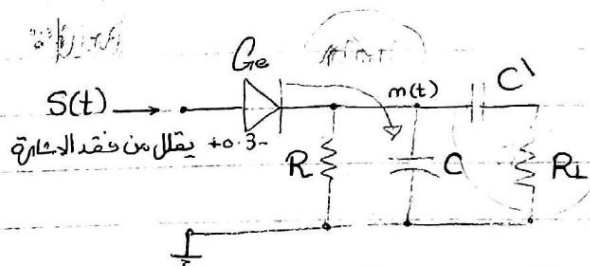
$$I_c = I_s + I_1 (m(t) - \underline{c(t)}) + I_2 (m^2 - \underline{2mc + c^2}) + \dots$$

$$s(t) = c(t) + k_a m(t) c(t)$$

Carrier + message * Carrier

using BPF that is tuned at f_c we will Pass the AM components.

(2) Demo



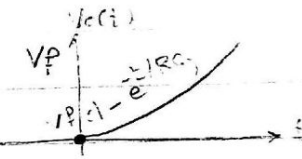
$R_1 \parallel R_2$ with smallest C $R_3 \parallel$ ripples
 $R = 100 \text{ k}\Omega$, largest C (C || C = sum) diagonal

- * Charging happens through R_s of the diode which is a very small resistance

$R_s \cdot C \downarrow \downarrow$ so charging happens fast which is required

Charging $V_c(t) = V_P (1 - e^{-t/RC})$

\hookrightarrow Final voltage or supply voltage



- * discharging through RC which is designed such that it is suitable value because:

- if RC is very small

$V_c(t) = V_s \cdot e^{-t/RC}$

\rightarrow RF ripples

Try 4.7 K Ω and 1 nF
or (4.7 || 10) K Ω and 1 nF
3.19 K Ω

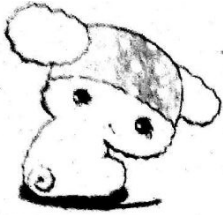
discharging $V_c = V_s \cdot e^{-t/RC}$

\hookrightarrow Supply voltage

- if RC is very large \rightarrow diagonal distortion

$\frac{1}{f_c} \ll RC \ll \frac{1}{f_m} \rightarrow$ optimum

$\frac{1}{465 \text{ kHz}} \ll 10 \text{ K}\Omega \cdot 1 \text{ nF} \ll \frac{1}{300}$
 $2.15 \times 10^{-3} \ll 10^{-5} \ll 3.33 \times 10^{-3}$



What is -ve Peak clipping?

due to C & R₁ part

at μ close to 1 \rightarrow no over modulation
while o/p look like



$$C(t) (1 + k_a \cdot m(t))$$

$I_{dc} \rightarrow$ see only R because C o.c

$I_{ac} \rightarrow$ see R || R₁

At f_c

I_{dc} sees different view than I_{ac}

In AM signal $I_{dc} < I_{ac}$

now \rightarrow I_{dc} may not be less than I_{ac} & it happens when μ close to 1

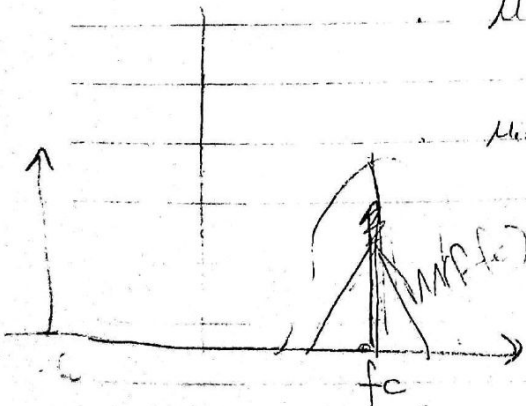
$$\mu = \frac{I_m}{I_c} = \frac{I_{ac}}{I_{dc}} = \frac{A_m/R_{ac}}{A_c/R_{dc}}$$

الطبيعي أنه يساوي $\frac{A_m}{A_c}$ لكن مع إضافة C، أصبح I_{dc} يرى R فقط بينما I_{ac} يرى R || R₁ وهي أصغر من R فلذلك زادت قيمة μ يعني I_m زادت عن A_m فلو تجاوز ال μ الواحد رغم عدم وصول μ إليه حدث -ve peak clipping

$$\mu = \frac{A_m}{A_c} \rightarrow \frac{I_m}{I_c} = \frac{I_m/R}{I_c/R}$$

$$\mu = \frac{I_m/R_{ac}}{I_c/R_{dc}} = \frac{I_m}{I_c} \cdot \frac{R_{dc}}{R_{ac}} \quad R_{ac} = C_o$$

$$= \frac{I_m}{I_c} \cdot \frac{R_{dc}}{R_{ac}}$$



Exp ⑤ FM modulation & demodulation



• In full AM (DSBTC), the B.W. of the AM signal was $2f_m$.

• In FM signals we have two types :

① NBFM (Narrow Band FM) \rightarrow B.W. = $2f_m$

② WBFM (Wide Band FM) \rightarrow B.W. = $2(\beta+1)f_m$
 $= 2(\Delta f_c + f_m)$

where $\beta = \frac{\Delta f}{f_m}$, $\Delta f = K_f \cdot A_m$

Modulation
index

\rightarrow Maximum frequency deviation

أقصى زيادة أو نقصان سيحدث في تردد
ال f_c بعد التعديل بواسطة f_m أو FM

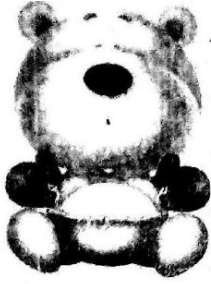
مثل μ في AM

• If $0 < \beta < 1 \rightarrow$ NBFM you will need only B.W. = $2f_m$

$\beta \gg 1 \rightarrow$ WBFM " " " " = $2(\beta+1)f_m$

• What's the benefit of FM over AM system & what are the drawbacks?

In NBFM \rightarrow Same AM B.W. which doesn't have benefit over AM in terms of less B.W. But as any FM signal it has high noise immunity because $m(t)$ is carried in the frequency of the carrier not in its amplitude. So, as noise only affects the signal amplitude, $m(t)$ will not be affected.



In WBFM \rightarrow B.W. $\xrightarrow{\text{WBFM}}$ B.W. AM which is

a drawback but still it has noise immunity

$m(t) \rightarrow$ Message Signal (Modulating Signal) الإشارة المُعدّلة
 $c(t) \rightarrow$ Carrier Signal
 $S(t) \rightarrow$ Modulated Signal الإشارة بعد التعديل

$S(t) = A_c \cos(\theta_i(t)) \rightarrow$ هو ال Carrier عندما تتغير له f
 مع الزمن بالتالي θ متغيرة مع الزمن و $m(t)$ و $m(t)$

$$\theta_i(t) = \int_0^t \omega_i(t) dt \quad \text{من تعريف ال } \theta$$

$$= 2\pi \int_0^t f_i(t) dt$$

$$= 2\pi \int_0^t f_c + K_f m(t) dt$$

التردد اللحظي وهو تردد $c(t)$ زائد تغير التردد ب $m(t)$

$$= 2\pi f_c t + 2\pi K_f \int_0^t m(t) dt$$

$$\therefore S(t) = A_c \cos(2\pi f_c t + 2\pi K_f \int_0^t m(t) dt)$$

$$f_i(t) = f_c + K_f \cdot m(t)$$

$$\cos u \xrightarrow{d/dt} -\sin u \cdot \frac{du}{dt}$$

At demodulation لاستخراج $m(t)$

$$\frac{d}{dt} S(t) = K \cdot \sin(2\pi f_c t + 2\pi K_f \int_0^t m(t) dt) \rightarrow \text{FM}$$

$$\rightarrow A_c \cdot 2\pi f_c + 2\pi K_f \cdot m(t) = 2\pi f_c \left(1 + \frac{K_f \cdot m(t)}{f_c}\right) \cdot A_c$$

\downarrow
AM

$$AM \rightarrow S(t) = A_c (1 + k_a m(t)) \cos(2\pi f_c t)$$



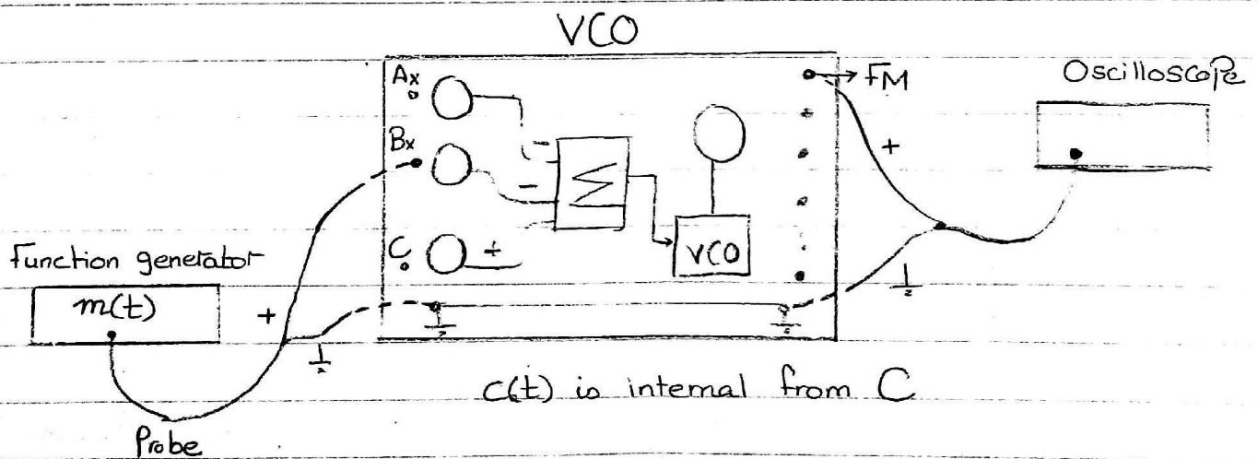
اذن المعادلة بعد التفاضل هي معادلة FM و AM فيستطيع
عمل detection بواسطة AM demodulator مثل ال
envelope detector

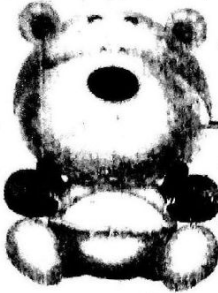
$$f_i(t) = f_c + k_f \cdot m(t)$$

$$f_i(t)_{\max} = f_c + |k_f \cdot m(t)|_{\max} = f_c + \boxed{k_f \cdot A_m} \rightarrow \Delta f$$

The Peak in case of sine, cosine
tri, square

① Modulation





Steps :-

الفكرة هو ضبط f_c أولاً عن طريق C حتى تكون $f_c = 465 \text{ KHz}$ ثم عمل التوصيلة السابقة وإدخال $m(t)$ على B_x وتفعيل $m(t)$ للبعد الداخل على VCO لتغيير التردد الخارج عن f_c

$$f_i(t) = f_c + k_f \cdot m(t) \quad \therefore \text{وهو المطلوب}$$

① Adjust C until $f_c = 465 \text{ KHz}$; at this point you must not connect B_x .

② Connect $m(t)$ from the f_n generator to B_x , choose $m(t)$ square wave , $f_m = 0.1 \text{ Hz}$

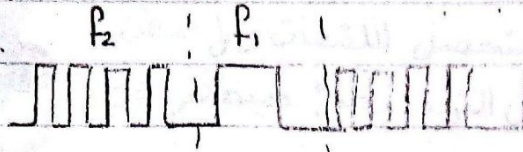
For 0.1 Hz frequency → ① choose the least range on f_n generator (2 Hz)

② Choose least freq; from the range
بتحرك $Knob$ لأقل قيمة وهاتكون
حوالي 1 أو 2 Hz

③ Press the $f \div 10$ button on the f_n generator

③ Let the B_x multiplier = 1 so you can see the effect of changing A_m through changing the amplitude by the f_n generator only.

Output :



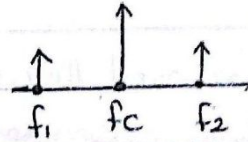
(لقطتين)

هام جداً :- * الإشارة الخارجة عبارة عن ترددين لأن الداخل هو Squam
به جهدين فقط $\pm A_m$

$$f_1 = f_c - k_f \cdot A_m \quad \text{التردد المنخفض}$$

$$f_2 = f_c + k_f \cdot A_m \quad \text{التردد العالي}$$

$$\Delta f = k_f \cdot A_m = \frac{f_2 - f_1}{2}$$

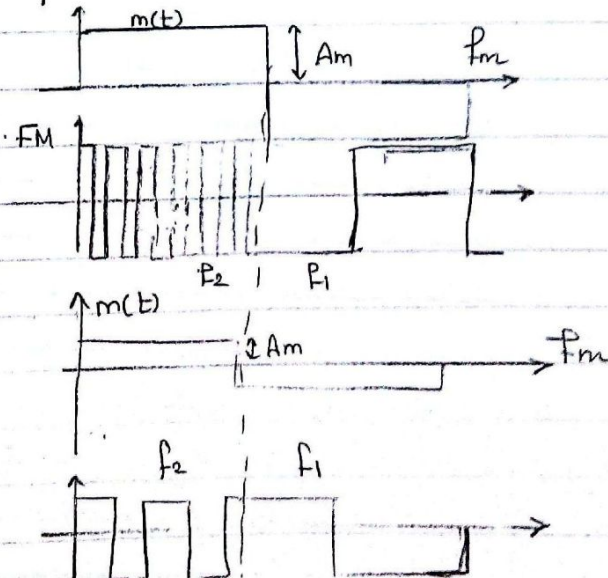


لقياس f_1 و f_2 على الـ analog osc. اضبط على $\frac{\Delta V}{\Delta t}$ مع أول ضغطه هيظهر خطين أفقيين
ضبطه مكان هيكونا رأسين : المفروض عند زمن دورى باستخدام الخطين دول وذلك باختبار خط منهم
* Study the effect of A_m , f_m .
ثم تحريكه صين ويسار بالـ Knob حتى بابة
ثم اختر الـ T وحرركه لنهاية T.

$$A_m \propto \Delta f$$

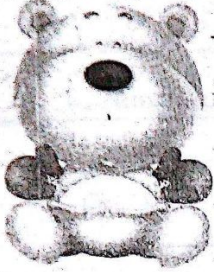
تؤثر في الفرق بين اللقطتين يعني $\Delta f \rightarrow (f_2 - f_1)$

هل التغير بين اللقطتين كبير أم أنهم متقاربين؟



When you're down and troubled
And you need some love care

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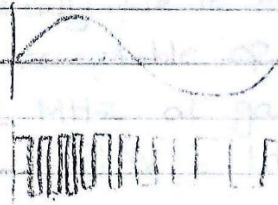


* P_m زمن عرض اللقطة \rightarrow التردد كبير هتحصل اللقطات ومار بعض
لما يكون بسرعة على عكس لو كان التردد بطيء هينظر كل
مشهد فترة أطول

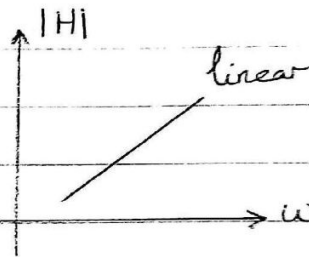
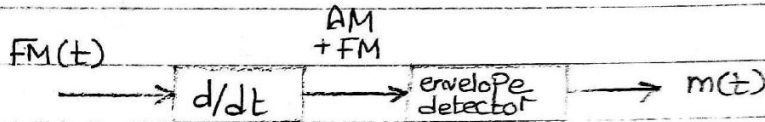
لو كان P_m كبير جداً ستظهر الإشارة ثابتة وبها التردد في نفس الوقت
وذلك لأنها تتغير فعلاً لكن بشكل سريع جداً صعب ملاحظته.



* IF the i/p was sine or tri, the o/p will have more than 2
frequencies, it will have infinite frequencies and the
freq. of the o/p will increase to a maximum then decrease.



② Demodulation



$H(\omega)$
شكل أدلة التفاضل

* We used to differentiate signals by op-amp circuit but this is not practical in FM signals differentiation, Why??

Because FM signals practically lie in the range $(88 \rightarrow 108)$ MHz which is out of the acceptable op-amp frequencies which has a maximum of 1 MHz. at gain = 1.

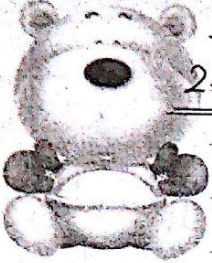
$$\text{Gain} * B.W = 10^6 \leftarrow \begin{array}{l} \text{قانون} \\ \text{opamp ال} \end{array}$$



أحيى هذه ال 4 دوائر قادرة على عمل التفاضل وسنعمل على أول نوع ال Slope detector

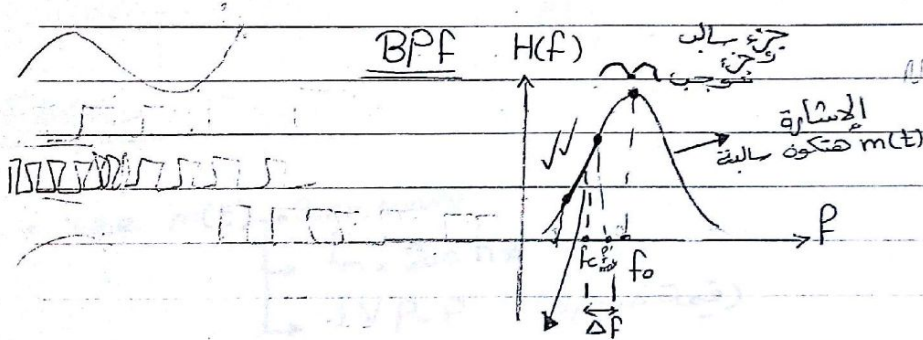
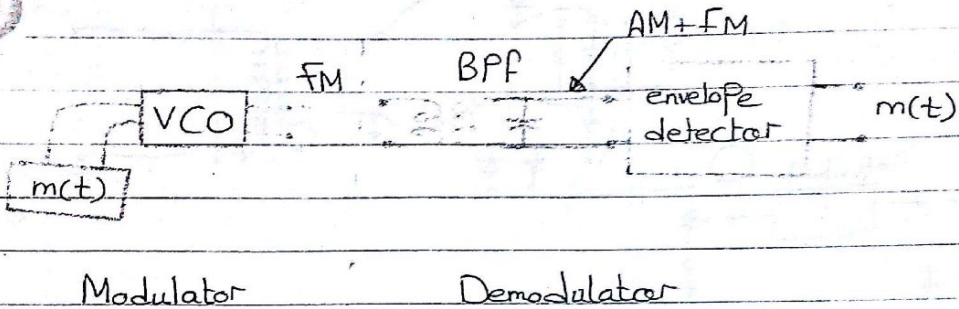
When you're down and troubled
And you need some love care

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2-1- Slope detector

* It is a tuned circuit (BPF)

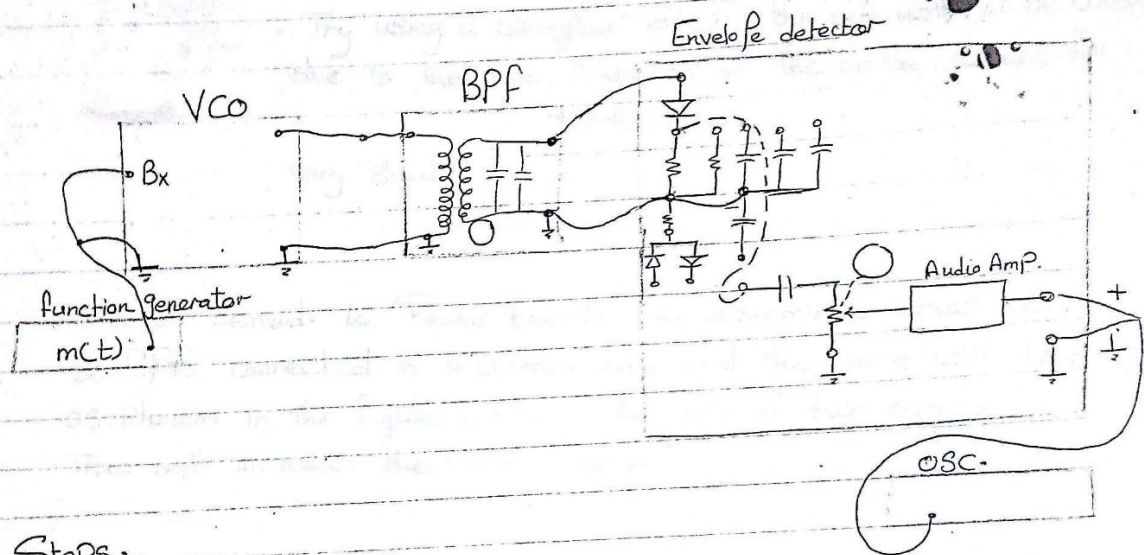


This is the Linear region we must work within
because we need Linear response in
differentiator circuits as stated previously.

* لماذا ستظهر $m(t)$ البقية في الجزء الآخر من المنحنى؟
لأن كل ما التردد هينزيد هيقبل ال amplitude (الميل سالب) وهذا عكس حبيباً
عل ال FM أن كل ما كان $m(t)$ تنزید منتزید $P_i(t)$ بالتالي هتظهر الإشارة
هنا مصروبة X سالب



You must step away from f_0 .



Steps:-

- Use $m(t)$ → Sine wave
 - $f_m = 200 \text{ Hz}$
 - 1 V_{p-p} (قيمة صينية)

• When displaying the o/p, the sine may be distorted so try to move away from f_c by two things

- ① Adjust f_c away by adjusting the knob in BPF
- ② decrease Δf by decreasing A_m

This will make the FM signal stay in the linear region of BPF curve

- You can try tuning until the distorted sine appear when f_c is at f_0

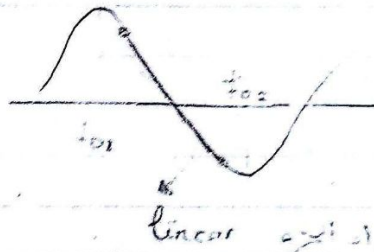
Don't worry.
Be happy

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- Try using a triangular $m(t)$, the o/p will not be linear due to the non-linearity of the curve except for very small Am.
Perfect

Another demod. is Round triwise freq. discriminator that has 2 BPFs connected in a certain way and the curve will look as shown in the figure which is the sum of two curves. This will increase the linear Region



Notes

• تذكر دائماً أن يكون الـ Gnd واحد لكل الـ modules مع الـ OSC. والـ Pn. generator

• للتأكد أن الخارج هو إشارة وليس noise غير شكل الـ $m(t)$ وراقب الشكل أمامك هل هيتغير أم لا ؟